

## Psychrometer Relationships

R.L. Snyder and K.T. Paw U

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### Introduction

These teaching notes discuss psychrometric relationships that are important for understanding humidity and its measurement. The first section discusses concepts related to measuring dry-bulb temperature. Then concepts pertaining to thermodynamic wet-bulb temperature are presented. Finally, some ideas on measuring the wet bulb temperature are discussed.

### Dry-bulb Temperature

The heat transfer to and from a dry-bulb thermometer depends on the long-wave radiation balance and sensible heat transfer. Assuming an emissivity  $e = 1.0$ , the net long-wave radiation can be expressed in terms of a resistance to radiation transfer ( $r_R$ ) in  $s\ m^{-1}$ .

$$R_{\text{net}} = \sigma(T_s^4 - T_t^4) = \rho C_p \frac{(T_s - T_t)}{r_R} \quad (1)$$

$T_s$  is the shield temperature (K) and  $T_t$  is the thermometer temperature (K).  $r$  is the air density ( $\text{kg}\ \text{m}^{-3}$ ) and  $C_p$  is the specific heat at constant pressure ( $\text{kJ}\ \text{kg}^{-1}\ \text{°C}^{-1}$ ). The

transfer of sensible heat by convection to and from the dry-bulb thermometer inside the shield is given by:

$$H = \rho C_p (T_t - T) r_H^{-1} \quad (2)$$

$H$  is the sensible heat to and from the thermometer and  $T$  is the air temperature within the shield. When in equilibrium,  $R_n = H$ , so

$$\rho C_p (T_s - T_t) r_R^{-1} = \rho C_p (T_t - T) r_H^{-1} \quad (3)$$

**REARRANGING, WE GET**

$$T_t = \frac{r_H T_s + r_R T}{r_R + r_H} \quad (4)$$

The goal is to have  $T_t$  be very close to  $T$ . This is accomplished by making:

- (1)  $r_H \ll r_R$  by using a very small thermometer or by ventilating more
- (2)  $T_s$  very close to  $T$  by painting the shield white, by insulating between outer and inner surfaces, or by increasing ventilation on both sides of the screen.

## Thermodynamic Wet-bulb Temperature

In an adiabatic system, the sum of latent and sensible heat remains constant. The initial, energy state is specified by the temperature ( $T$ ), vapor pressure ( $e$ ), and total pressure ( $p$ ). If liquid water is present and  $e$  is smaller than  $e_s(T)$ , then water will evaporate and both  $e$  and  $p$  will increase. Assuming no exchange of heat between the system and the outside environment, an increase of latent heat in the system, represented by an increase in  $e$ , must be balanced by a decrease in sensible heat, represented by a decrease in  $T$ . This process will continue until the air becomes saturated at  $T'$  (the thermodynamic wet-bulb temperature). The corresponding saturation vapor pressure is  $e_s(T')$ . The initial water vapor density, defined by  $T$  and  $e$ , is

$$\varepsilon \left( \frac{e}{p} \right) \rho = \frac{M_v}{M_d} \left( \frac{e}{p} \right) \rho \quad \text{kg m}^{-3} \quad (5)$$

where,  $M_v$  and  $M_d$  are the molecular weights ( $\text{kg mol}^{-1}$ ) of dry air and water vapor, respectively,  $e$  is the vapor pressure,  $p$  is the barometric pressure, and  $r$  is the dry air

density. When the vapor pressure rises from  $e$  to  $e_s(T')$ , the change in latent heat per unit volume is

$$\lambda_E \left( \frac{e_s(T') - e}{p} \right) \rho \quad \text{kJ m}^{-3} \quad (6)$$

where  $l$  is the latent heat of vaporization ( $\text{kJ kg}^{-1}$ ). The corresponding sensible heat used for vaporizing the water is

$$\rho C_p (T - T') \quad \text{kJ m}^{-3} \quad (7)$$

Equating the two expressions and solving for  $e$ , we get

$$e = e_s(T') - \frac{C_p p}{\lambda_E} (T - T') \quad \text{kPa} \quad (8)$$

where  $\gamma = \frac{C_p p}{\lambda_E}$  is the psychrometric constant. Actually,  $g$  is not a constant but a function of barometric pressure ( $p$ ), which depends on elevation and passing weather systems and on the latent heat of vaporization ( $l$ ), which is a weak function of temperature. If  $p = 101.3$  kPa, then  $g = 0.066$  at  $0^\circ\text{C}$  and  $g = 0.067$  at  $20^\circ\text{C}$ . A good formula to estimate  $p$  is

$$p = 101.3 \left( \frac{293 - 0.0065E}{293} \right)^{5.26} \quad \text{kPa} \quad (9)$$

To estimate  $l$ , use

$$\lambda = 2.501 - 0.002361T \quad \text{J kg}^{-1} \quad (10)$$

Note that vapor pressure can also be determined from  $e_s(T)$  rather than  $e_s(T')$ . Using the slope of the saturation vapor pressure curve at the mean of the air and wet-bulb temperatures ( $D$ ), small changes in saturation vapor pressure are expressed as:

$$e_s(T') = [e_s(T) - \Delta'(T - T')] \quad \text{kPa} \quad (11)$$

Substituting into the psychrometric equation (Eq. 8), we get

$$e = e_s(T) - (\Delta' + \gamma)(T - T') \quad \text{kPa} \quad (12)$$

Substituting the slope of the saturation vapor pressure curve at air temperature ( $D$ ) for  $D$ , and solving for  $T'$  provides an equation to estimate the wet-bulb temperature.

$$T' = T - \frac{e_s(T) - e}{\Delta + \gamma} \quad ^\circ\text{C} \quad (13)$$

The error in using  $D$  rather than  $D\phi$  is small when  $T - T'$  is small, but the error increases with greater wet-bulb depression.

## Measured Wet-bulb Temperature

The measured wet-bulb temperature ( $T_w$ ) is an estimate of the thermodynamic wet-bulb temperature ( $T'$ ). For a wet-bulb thermometer with temperature ( $T_w$ ) when exposed to air at temperature ( $T$ ) and surrounded by a radiation shield at air temperature, the rate of sensible heat gain ( $H$ ) and net radiation ( $R_n$ ) can be expressed as

$$R_n + H = \frac{\rho C_p (T - T_w)}{r_{HR}} \quad \text{kJ m}^{-2}\text{s}^{-1} \quad (14)$$

where  $r_{HR}$  is the parallel resistance to convective and radiation heat transfer. The rate of latent heat loss from the wet-bulb is

$$\lambda E = \frac{\lambda \epsilon \rho}{p} \left( \frac{e_s(T_w) - e}{r_v} \right) \quad \text{kJ m}^{-2}\text{s}^{-1} \quad (15)$$

Recall that the psychrometric constant is

$$\gamma = \frac{C_p p}{\lambda \epsilon} \quad \text{so} \quad \frac{1}{\gamma} = \frac{\lambda \epsilon}{C_p p} \quad \text{and} \quad \frac{C_p}{\gamma} = \frac{\lambda \epsilon}{p} \quad (16)$$

By substitution, we get

$$\lambda E = \frac{\rho C_p (e_s(T_w) - e)}{\gamma r_v} \quad (17)$$

In equilibrium,  $\lambda E = R_n + H$ , so

$$\frac{\rho C_p (e_s(T_w) - e)}{\gamma r_v} = \frac{\rho C_p (T - T_w)}{r_{HR}} \quad (18)$$

then

$$\frac{\rho C_p (e_s(T_w) - e)}{\gamma r_v} = \frac{\rho C_p (T - T_w)}{r_{HR}} \quad (19)$$

and

$$e = e_s(T_w) - \gamma \left( \frac{r_v}{r_{HR}} \right) (T - T_w) \quad (20)$$

Thus, the wet-bulb temperature equals the thermodynamic wet-bulb temperature only when  $r_v = r_{HR}$ . The actual equation to estimate  $e$  is

$$e = e_s(T_w) - \gamma^* (T - T_w) \quad (21)$$

where  $\gamma^* = \gamma \left( \frac{r_v}{r_{HR}} \right)$ . Based on the concepts of forced convection, the resistance to vapor transfer equals 93% of the resistance to convective heat transfer ( $r_v = 0.93 r_H$ ) for an aspirated wet-bulb thermometer at 20°C. When  $g = g^*$ , then the resistance to vapor transfer equals the parallel resistance to convective and radiative heat transfer. Therefore,

$$\frac{1}{r_v} = \frac{1}{r_{HR}} = \frac{1}{r_H} + \frac{1}{r_R} = \frac{1}{0.93r_H} \quad (22)$$

Rearranging terms, we get

$$\frac{1}{r_R} = \frac{1 - 0.93}{0.93r_H} \quad (23)$$

and

$$r_H = \frac{0.07}{0.93} r_R = 0.075 r_R \quad (24)$$

For example, if  $r_R = 210 \text{ s m}^{-1}$ , then  $r_H = 17 \text{ s m}^{-1}$ . Then the measured wet-bulb temperature is bigger than the thermodynamic wet-bulb temperature if  $r_H > 17 \text{ s m}^{-1}$ . The measured wet-bulb is smaller when  $r_H < 17 \text{ s m}^{-1}$ . Therefore, if a thermometer with  $r_R = 210 \text{ s m}^{-1}$  is ventilated so that  $r_H \gg 17 \text{ s m}^{-1}$ , the measured will approximately equal the thermodynamic wet-bulb temperature. The radiation resistance is mainly affected by the thermometer size and shielding. Resistance to sensible heat transfer is mainly affected by ventilation.

