

# Penman-Monteith daily (24-hour) Reference Evapotranspiration Equations for Estimating $ET_o$ , $ET_r$ and HS $ET_o$ with Daily Data

Copyright (2002) Regents of the University of California

Created January 6, 2002

Revised February 2009

R. L. Snyder, Biometeorology Specialist  
Department of Land, Air and Water Resources  
University of California  
Davis, CA 95616, USA

S. Eching, Senior Land and Water Use Scientist  
California Department of Water Resources  
Office of Water Use Efficiency

P.O. Box 942836  
Sacramento, CA 94236, USA

## Overview

The following text is a description of the steps needed to estimate reference evapotranspiration ( $ET_{ref}$ ) for a 0.12 m tall reference surface ( $ET_{os}$ ) and for a 0.50 m tall reference surface ( $ET_{rs}$ ) using daily weather data as adopted by the Environmental Water Resources Institute - American Society of Civil Engineers (ASCE-EWRI, 2004). Note that the steps are in the same sequence as one would use when write computer code. The symbols were shortened to  $ET_o$  and  $ET_r$  in this documentation. The Hargreaves-Samani (1982); Hargreaves-Samani (1985) equation for estimating  $ET_o$  are also presented and the symbol used is  $ET_h$

## Data Requirements

Site characteristics including the latitude (+ for north and – for south) and elevation (m) above sea level must be input. The required weather data includes hourly solar radiation ( $\text{MJ m}^{-2}\text{d}^{-1}$ ), maximum and minimum air temperature ( $^{\circ}\text{C}$ ), mean wind speed ( $\text{m s}^{-1}$ ) and mean dew point temperature ( $^{\circ}\text{C}$ ). The air and dew point temperatures should be measured at between 1.5 and 2.0 m height and the wind speed should be measured at 2.0 m height. For wind speeds measured at some height other than 2.0 m, the wind speed at 2 m height ( $u_2$ ) can be estimated as:

$$u_2 = u_z \left( \frac{4.87}{\ln(67.8z_w - 5.42)} \right)$$

where  $u_z$  = wind speed ( $\text{m s}^{-1}$ ) at height  $z_w$  (m) above the ground.

The following text is a description of the steps needed to estimate reference evapotranspiration for a 0.12 m tall reference surface using daily weather data as adopted by the American Society of Civil Engineers (ASCE-EWRI, 2004). The steps are in the same sequence as one would enter code into a computer program.

**STEP 1: Extraterrestrial radiation ( $R_a$ ) is calculated for each day using the following equations from Duffie and Beckman (1980).**

$G_{SC}$  = solar constant in  $\text{MJ m}^{-2} \text{min}^{-1}$

$$G_{SC} = 0.082$$

$\sigma$  = Steffan-Boltzman constant in  $\text{MJ m}^{-2} \text{d}^{-1} \text{K}^{-4}$

$$\sigma = 4.90 \times 10^{-9}$$

$\phi$  = latitude in radians converted from latitude ( $L$ ) in degrees

$$\phi = \frac{\pi L}{180}$$

$d_r$  = correction for eccentricity of Earth's orbit around the sun on day  $i$  of the year

$$d_r = 1 + 0.033 \cos\left(\frac{2\pi}{365} i\right) \quad (1)$$

$\delta$  = declination of the sun above the celestial equator in radians on day  $i$  of the year

$$\delta = 0.409 \sin\left(\frac{2\pi}{365} i - 1.39\right) \quad (2)$$

$\omega_s$  = sunrise hour angle in radians

$$\omega_s = \cos^{-1}[-\tan \phi \tan \delta] \quad (3)$$

$R_a$  = extraterrestrial radiation ( $\text{MJ m}^{-2} \text{d}^{-1}$ )

$$R_a = \left(\frac{24 \cdot 60}{\pi}\right) G_{SC} d_r [\omega_s \sin \delta \sin \phi + \cos \phi \cos \delta \sin \omega_s] \quad (4)$$

**STEP 2: Calculate the daily net radiation ( $R_n$ ) expected over grass in  $\text{MJ m}^{-2} \text{d}^{-1}$  using equations from Allen et al. (1994).**

$R_{so}$  = clear sky total global solar radiation at the Earth's surface in  $\text{MJ m}^{-2} \text{d}^{-1}$

$$R_{so} = R_a (0.75 + 2.0 \times 10^{-5} E_t) \quad (5)$$

$R_{ns}$  = net solar radiation over grass as a function of measured solar radiation ( $R_s$ ) in  $\text{MJ m}^{-2} \text{d}^{-1}$

$$R_{ns} = (1 - 0.23) R_s \quad (6)$$

$f$  = a cloudiness function of  $R_s$  and  $R_{so}$

$$f = 1.35 \frac{R_s}{R_{so}} - 0.35 \quad (7)$$

$e_s(T_x)$  = saturation vapor pressure (kPa) at the maximum daily air temperature ( $T_x$ ) in  $^{\circ}\text{C}$

$$e_s(T_x) = 0.6108 \exp\left(\frac{17.27 T_x}{T_x + 237.3}\right) \quad (8)$$

$e_s(T_n)$  = saturation vapor pressure (kPa) at the minimum daily air temperature ( $T_n$ ) in  $^{\circ}\text{C}$

$$e_s(T_n) = 0.6108 \exp\left(\frac{17.27 T_n}{T_n + 237.3}\right) \quad (9)$$

$e_d$  = actual vapor pressure or saturation vapor pressure (kPa) at the mean dew point temperature from the daily maximum ( $T_x$ ) and minimum ( $T_n$ ) temperature ( $^{\circ}\text{C}$ ) and maximum ( $RH_x$ ) and minimum ( $RH_n$ ) relative humidity (%).

$$e_d = \frac{e_s(T_x) \frac{RH_n}{100} + e_s(T_n) \frac{RH_x}{100}}{2} \quad (10)$$

$e_d$  = actual vapor pressure or saturation vapor pressure (kPa) at the daily mean dew point ( $T_d$ ) temperature.

$$e_d = e_s(T_d) = 0.6108 \exp\left(\frac{17.27T_d}{T_d + 237.3}\right) \quad (11)$$

$\varepsilon'$  = apparent 'net' clear sky emissivity

$$\varepsilon' = 0.34 - 0.14\sqrt{e_a} \quad (12)$$

Note that  $\varepsilon' = \varepsilon_{vs} - \varepsilon_a$ , where  $\varepsilon_{vs}$  is the emissivity of the grass and  $\varepsilon_a$  is the emissivity from the atmosphere. It is called 'apparent' because the temperature from a standard shelter rather than the surface temperature and atmosphere temperature are used to calculate the 'net' long-wave radiation balance. Equation 11 is called the 'Brunt form' equation for net emittance because the form of the equation is similar to Brunt's equation for apparent long-wave emissivity from a clear sky.

$R_{nl}$  = net long wave radiation in  $\text{MJ m}^{-2} \text{d}^{-1}$

$$R_{nl} = -f \varepsilon' \sigma \left[ \frac{(T_x + 273.15)^4 + (T_n + 273.15)^4}{2} \right] \quad (13)$$

$R_n$  = net radiation over grass in  $\text{MJ m}^{-2} \text{d}^{-1}$

$$R_n = R_{ns} + R_{nl} \quad (14)$$

### STEP 3: Calculate variables needed to compute $ET_h$ , $ET_o$ and $ET_r$ .

$\beta$  = barometric pressure in kPa as a function of elevation ( $E_l$ ) in meters

$$\beta = 101.3 \left( \frac{293 - 0.0065E_l}{293} \right)^{5.26} \quad (15)$$

$\lambda$  = latent heat of vaporization in ( $\text{MJ kg}^{-1}$ )

$$\lambda = 2.45 \quad (16)$$

$\gamma$  = psychrometric constant in  $\text{kPa } ^\circ\text{C}^{-1}$

$$\gamma = 0.00163 \frac{\beta}{\lambda} \quad (17)$$

$T_m$  = mean daily temperature in  $^\circ\text{C}$

$$T_m = \frac{T_x + T_n}{2} \quad (18)$$

$e^o$  = saturation vapor pressure at  $T_m$

$$e^o = 0.6108 \exp\left(\frac{17.27T_m}{T_m + 237.3}\right) \quad (19)$$

$\Delta$  = slope of the saturation vapor pressure curve ( $\text{kPa } ^\circ\text{C}^{-1}$ ) at mean air temperature ( $T_m$ )

$$\Delta = \frac{4099e^o}{(T_m + 237.3)^2} \quad (20)$$

$G$  = soil heat flux density in  $\text{MJ m}^{-2} \text{d}^{-1}$

$$G \approx 0 \quad (21)$$

$e_a$  = mean of the  $T_x$  and  $T_n$  saturation vapor pressures (kPa)

$$e_a = \frac{e_s(T_x) + e_s(T_n)}{2} \quad (22)$$

**STEP 4: Calculate  $ET_h$  using the Hargreaves-Samani (1982); Hargreaves-Samani (1982) equation.**

Hargreaves-Samani equation for ET of a short, 0.12 m tall reference surface

$$ET_h = 0.408(0.0023R_a[T_m + 17.8]\sqrt{T_x - T_n}) \quad (23)$$

where the 0.408 = 1/λ factor converts from MJ m<sup>-2</sup>d<sup>-1</sup> to mm d<sup>-1</sup>.

**STEP 5: Calculate  $ET_o$  using the ASCE-EWRI (2004) standardized equation for short canopy reference ET.**

$R_o$  = radiation term of the Penman-Monteith equation for short canopy reference ET with  $U_2$  the wind speed at 2 m height

$$R_o = \frac{0.408\Delta(R_n - G)}{\Delta + \gamma(1 + 0.34U_2)} \quad (24)$$

where 0.408=1/2.45 converts the units from MJ m<sup>-2</sup> d<sup>-1</sup> to mm d<sup>-1</sup>.

$A_o$  = aerodynamic term of the Penman-Monteith equation for short canopy reference ET with  $u_2$  the wind speed at 2 m height

$$A_o = \frac{\left(\frac{900\gamma}{T_M + 273}\right)U_2(e_a - e_d)}{\Delta + \gamma(1 + 0.34U_2)} \quad (25)$$

Standardized Reference Evapotranspiration for a short, 0.12 m reference surface in mm d<sup>-1</sup>.

$$ET_o = R_o + A_o \quad (26)$$

**STEP 6: Calculate  $ET_r$  using the ASCE-EWRI (2004) standardized equation for tall canopy reference ET.**

$R_r$  = radiation term of the Penman-Monteith equation for tall canopy reference ET with  $U_2$  the wind speed at 2 m height

$$R_r = \frac{0.408\Delta(R_n - G)}{\Delta + \gamma(1 + 0.38U_2)} \quad (27)$$

$A_r$  = aerodynamic term of the Penman-Monteith equation for tall canopy reference ET with  $u_2$  the wind speed at 2 m height

$$A_r = \frac{\left(\frac{1600\gamma}{T_M + 273}\right)U_2(e_a - e_d)}{\Delta + \gamma(1 + 0.38U_2)} \quad (28)$$

Standardized Reference Evapotranspiration for a tall, 0.5 m reference surface in mm d<sup>-1</sup>.

$$ET_r = R_r + A_r \quad (29)$$

## REFERENCES

- Allen, R.G., M.E., Jensen, J.L. Wright, and R.D. Burman. 1989. Operational estimates of evapotranspiration. *Agron. J.* 81:650-662.
- Allen, R.G., M. Smith, L.S. Pereira, A. Perrier. 1994. An update for the calculation of reference evapotranspiration. *ICID Bulletin* 1994 Vol 43 No 2.
- Allen, R.G., Walter, I.A., Elliott, R., Mecham, B., Jensen, M.E., Itenfisu, D., Howell, T.A., Snyder, R., Brown, P., Eching, S., Spofford, T., Hattendorf, M., Cuenca, R.H., Wright, J.L., and Martin, D. 2000. Issues, requirements and challenges in selecting and specifying a standardized ET equation. ASCE.
- Allen, R.G., Walter, I.A., Elliott, R.L., Howell, T.A., Itenfisu, D., Jensen, M.E. and Snyder, R.L. 2005. *The ASCE Standardized Reference Evapotranspiration Equation*. Amer. Soc. of Civil Eng. Reston, Virginia. 192p.
- ASCE-EWRI. 2004. The ASCE Standardized Reference Evapotranspiration Equation. Technical Committee report to the Environmental and Water Resources Institute of the American Society of Civil Engineers from the Task Committee on Standardization of Reference Evapotranspiration. 173 p.
- Doorenbos, J. and W.O. Pruitt. 1977. Crop Water Requirements. FAO Irrigation and Drainage Paper 24, United Nation Food and Agriculture Organization, Rome.
- Duffie, J.A. and W.A. Beckman. 1980. *Solar engineering of thermal processes*. John Wiley and Sons, New York. pp. 1-109.
- Hargreaves, G.H., and Samani, Z.A. (1982). "Estimating potential evapotranspiration." Tech. Note, *J. Irrig. and drain. Engrg.*, ASCE, 108(3):225-230.
- Hargreaves, G.H., and Samani, Z.A. (1985). "Reference crop evapotranspiration from temperature." *Applied Eng. in Agric.*, 1(2):96-99.
- Jensen, M.E., R.D. Burman, and R.G. Allen, Eds. 1990. Evapotranspiration and Irrigation Water Requirements. Amer. Soc. of Civil Eng., New York.
- Smith, M. 1991. Report on the expert consultation on procedures for revision of FAO Guidelines for prediction of crop water requirements. United Nations - Food and Agriculture Organization, Rome, Italy
- Tetens, V.O. 1930. Uber einige meteorologische. Begriffe, *Zeitschrift fur Geophysik.* 6:297-309.
- Walter, I.A., R.G. Allen, R. Elliott, M.E. Jensen, D. Itenfisu, B. Mecham, T.A. Howell, R. Snyder, P. Brown, S. Eching, T. Spofford, M. Hattendorf, R.H. Cuenca, J.L. Wright, D. Martin. 2000. ASCE's Standardized Reference Evapotranspiration Equation. Proc. of the Watershed Management 2000 Conference, June 2000, Ft. Collins, CO, American Society of Civil Engineers, St. Joseph, MI.